

2.29 Numerical Fluid Mechanics Fall 2009 – Special Lecture 2

Discontinuous Galerkin Finite Element Methods

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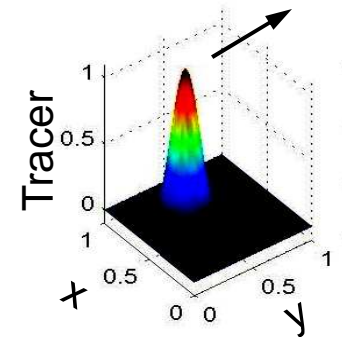
MSEAS Group

Department of Mechanical Engineering

Massachusetts Institute of Technology

- Background/Motivation
 - Scalar Advection
 - Lock Exchange Problem
 - High-Order on unstructured meshes
- Definitions and Notation
- Method of Weighted Residuals – Comparison to FV
- Concept of Basis and Test Functions
 - Types of test functions
 - Types of basis functions
 - Continuous versus Discontinuous
- Worked example
- Difficulties and future research

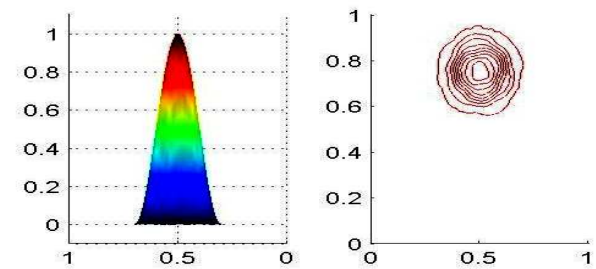
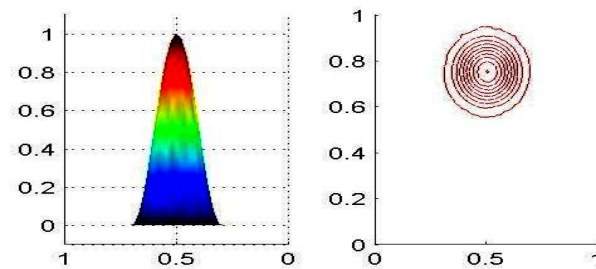
- DG Advantages
 - Localized memory access
 - Higher order accuracy
 - Well-suited to adaptive strategies
 - Designed for advection dominated flows
 - Excellent for wave propagation
 - Can be used for complex geometries
- DG Disadvantages
 - Expensive?
 - Difficult to implement
 - Difficulty in treating higher-order derivatives



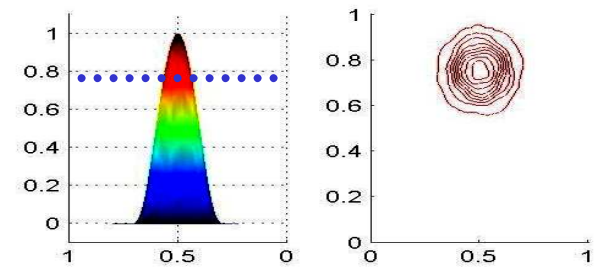
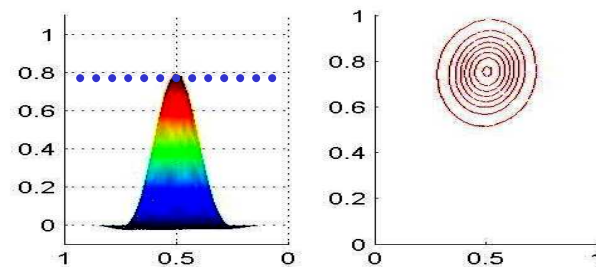
Low Order
 $p=1$, Time=260s, DoF=10,300

High Order
 $p=6$, Time=100s, DoF=6,300

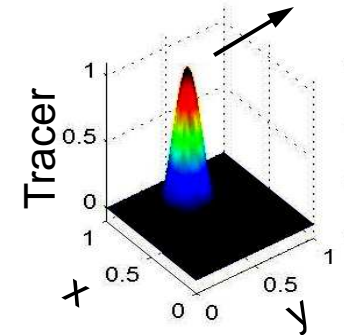
Initial Condition



Final Condition



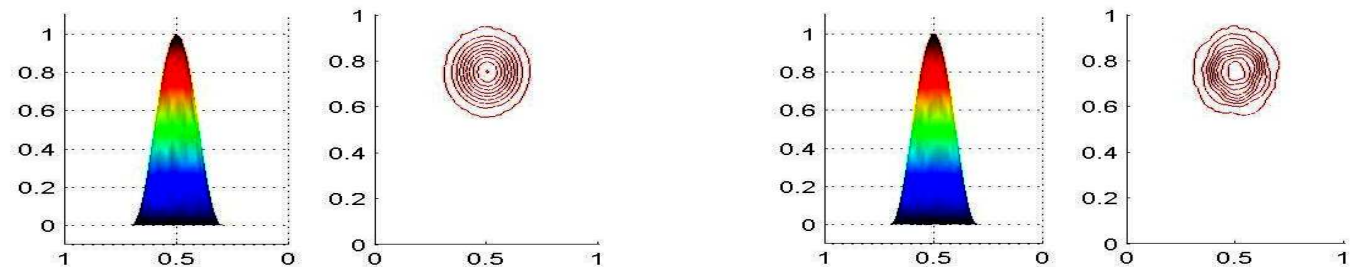
- Less Numerical Diffusion/Dissipation
- Higher accuracy for lower computational time
- Example test case: 20 periods of linear tracer advection:



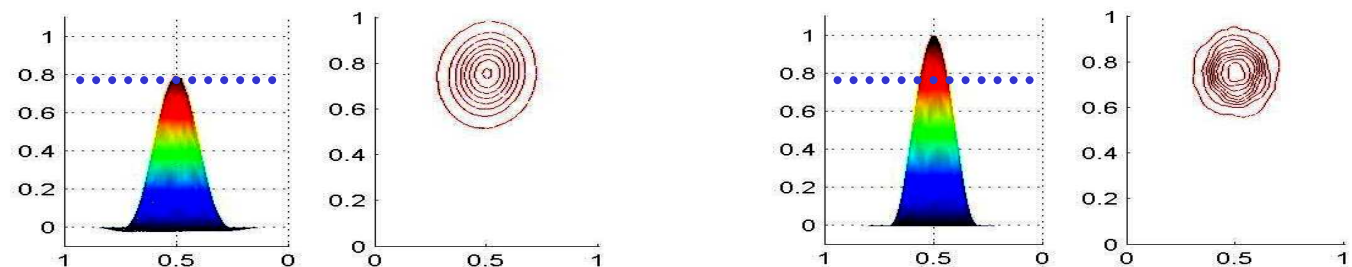
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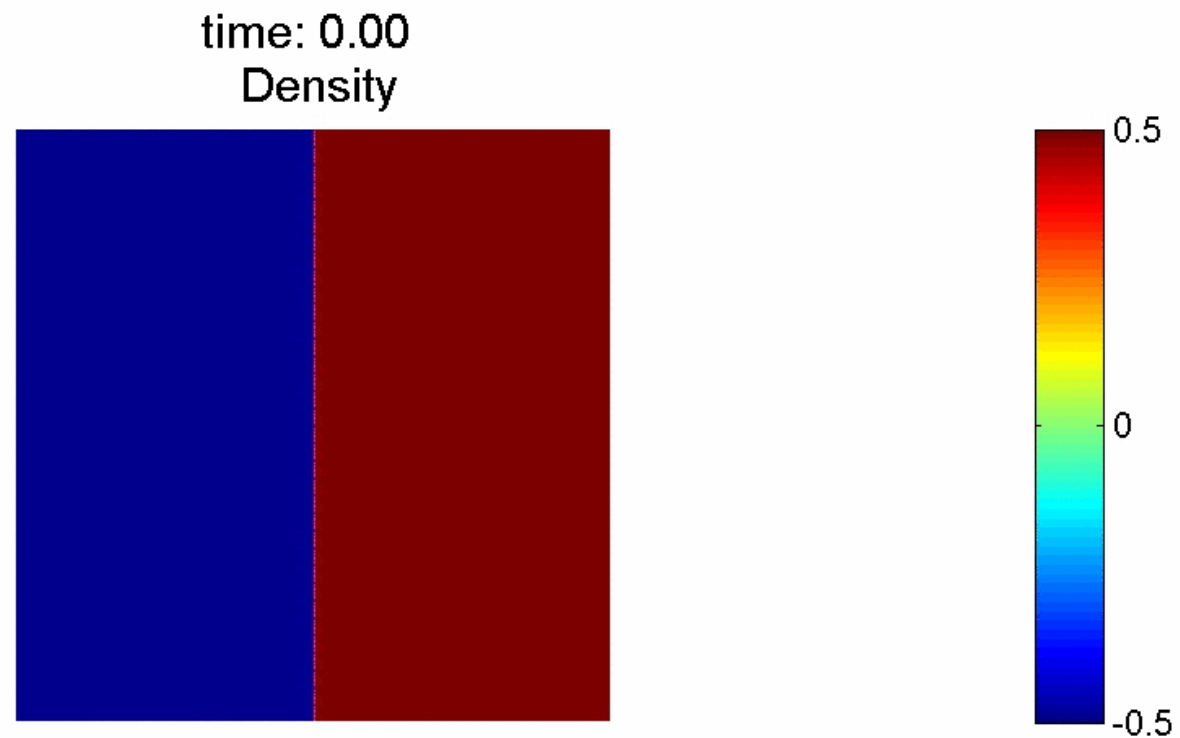
Initial Condition



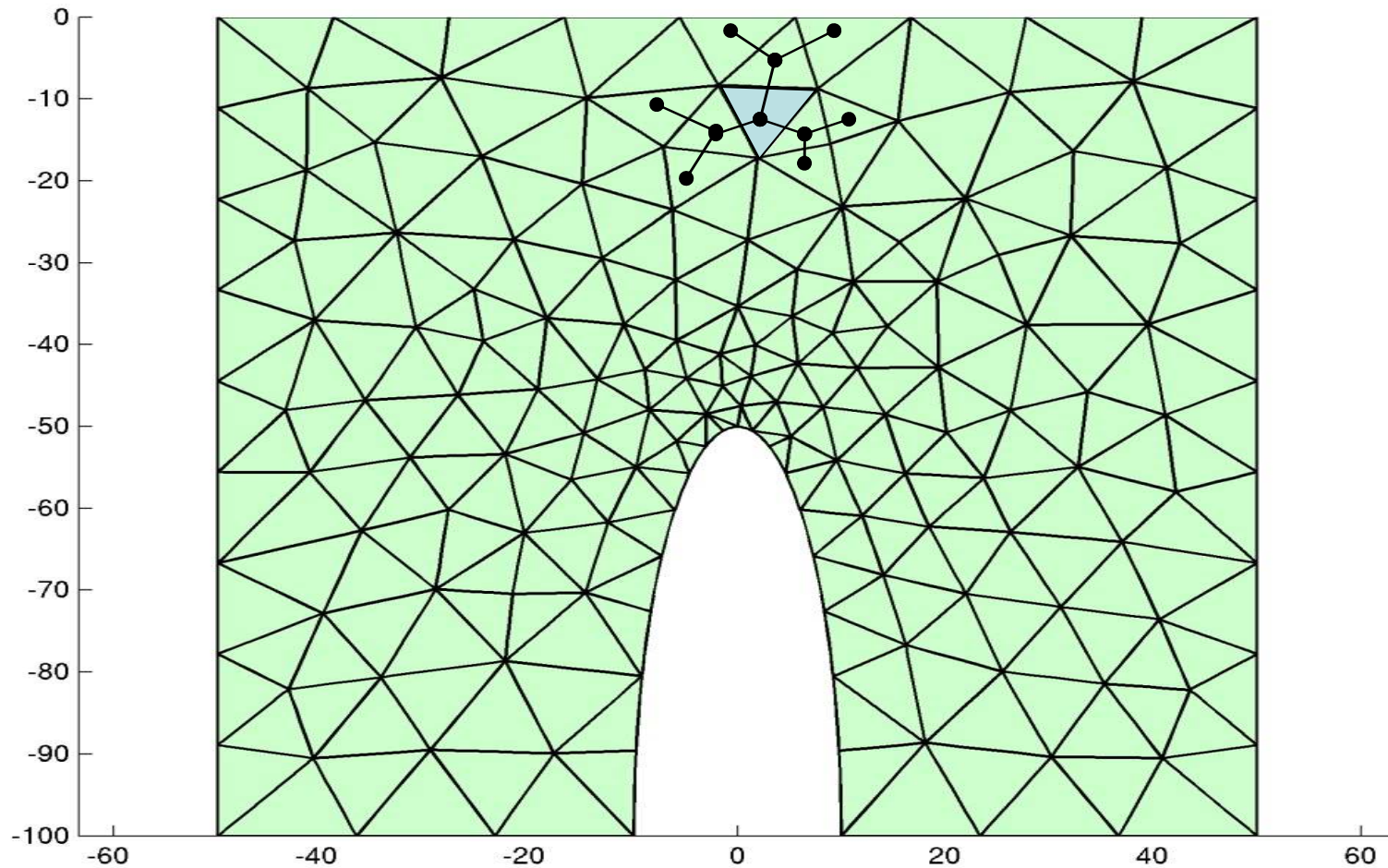
Final Condition

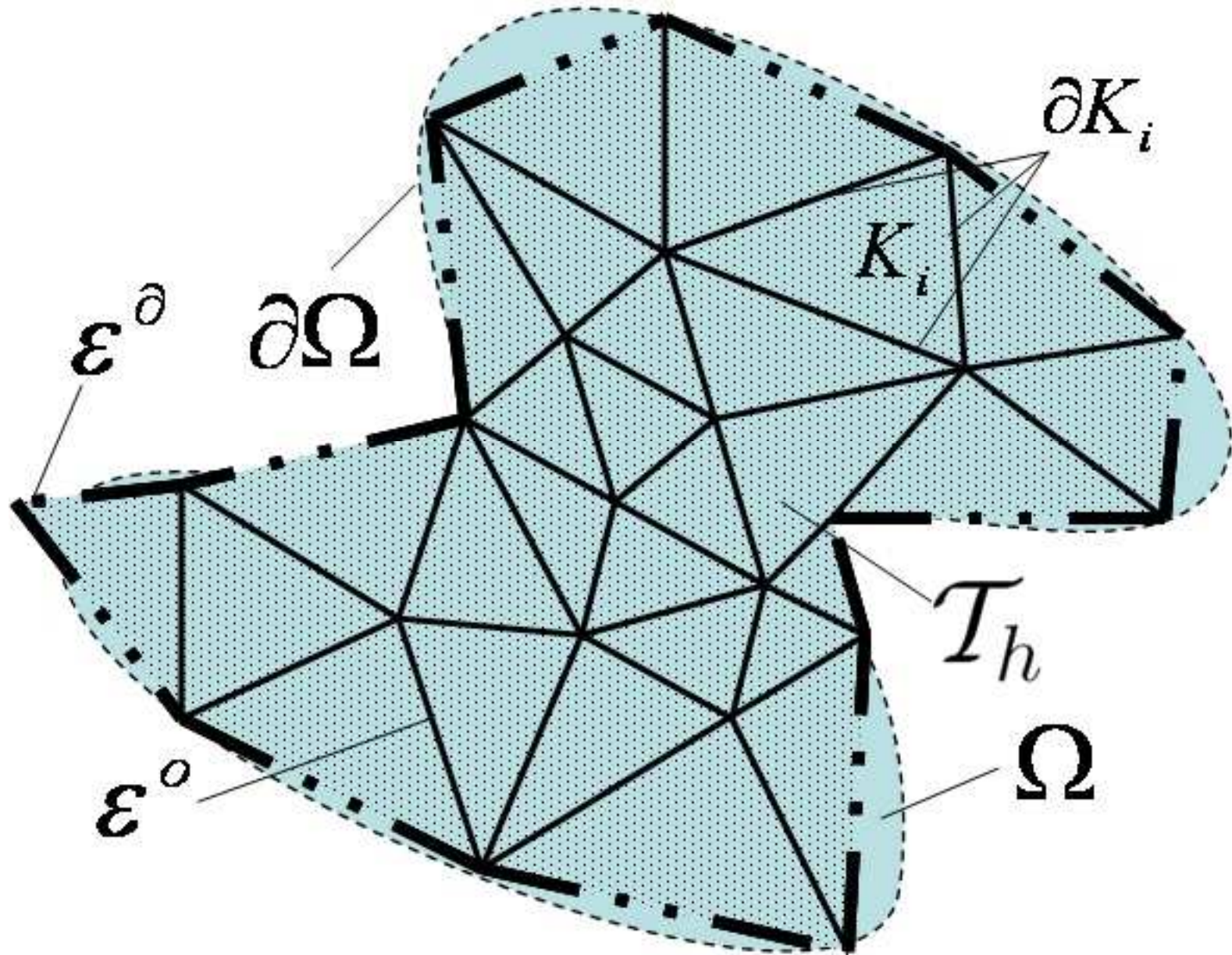


- 5th order elements
- 35 x 35 elements (equivalent to approx 230x230 FV)



- Large Stencils are difficult
 - What to do at boundaries?





- General advection equation

$$\frac{\partial u}{\partial t} + \nabla \cdot \mathbf{F}(u) = S(u), \quad \text{in } (0, T) \times \Omega$$

$$u = g_D, \quad \text{on } \partial\Omega_D$$

$$\mathbf{F}(u) \cdot \hat{\mathbf{n}} = g_N, \quad \text{on } \partial\Omega_N$$

$$u = u_0, \quad \text{in } (0, 0) \times \Omega$$

- Multiply residual by test function
- Integrate over domain
- Set equal to zero

$$\int_K \left\{ \frac{\partial u_h}{\partial t} w + [\nabla \cdot \mathbf{F}(u_h)] w \right\} dK = \int_K S(u_h) w dK, \quad \forall K \in \mathcal{T}_h$$

- Integrate by parts

$$\int_K \frac{\partial u_h}{\partial t} w dK + \int_K \nabla \cdot [\mathbf{F}(u_h) w] dK - \int_K \mathbf{F}(u_h) \cdot \nabla w dK = \int_K S(u_h) w dK$$

- Divergence theorem (weak form)

$$\int_K \frac{\partial u_h}{\partial t} w dK + \int_{\partial K} \hat{\mathbf{F}}(u_h) \cdot \hat{\mathbf{n}} w d\partial K - \int_K \mathbf{F}(u_h) \cdot \nabla w dK = \int_K S(u_h) w dK$$

- If test function is in infinite space
 - Exact minimization of residual
- Discretization of equations leads to finite test function space

$$W_h^p = \{w \in L^2(\Omega) : w|_K \in \mathcal{P}^p(K), \forall K \in \mathcal{T}_h\}$$

w in L2 such that w restricted to K in polynomial space of order p, for all K in triangulation

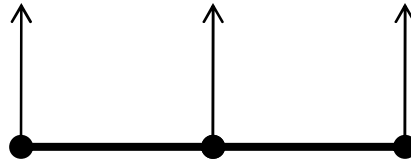
- Two spaces, the normed L^2 space and Hilbert space

- DG -- L^2 : $\int_{\Omega} f(x)^2 d\Omega < \infty$

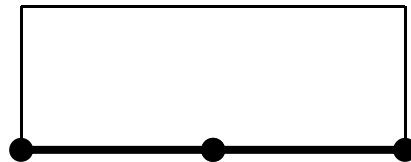
- CG -- H^1 : $\int_{\Omega} f(x)^2 + \nabla f(x) \cdot \nabla f(x) d\Omega < \infty$

- Is x^2+x+1 in L^2 ? What about H^1 ? How about $\delta(x)$?

- Collocation



- Subdomain



- Galerkin
 - Test function is chosen to be the same as the basis function
 - Often used in practice

- If basis in infinite space and test function in infinite space
 - Solution will be exact

$$u(\mathbf{x}, t) \approx u_h(\mathbf{x}, t) = \sum_i u_{h,i}(t) \theta_i(\mathbf{x})$$

$$u_h(\mathbf{x}, t) = \sum_{i=1}^{N_P} u_{h,i}(t) \psi_i(\mathbf{x})$$

$$u_h(\mathbf{x}, t) = \sum_{i=1}^{N_P} u_{h,i}(t, \mathbf{x}_i) \phi_i(\mathbf{x})$$

- Einstein Notation

$$u \approx u_i \theta_i$$

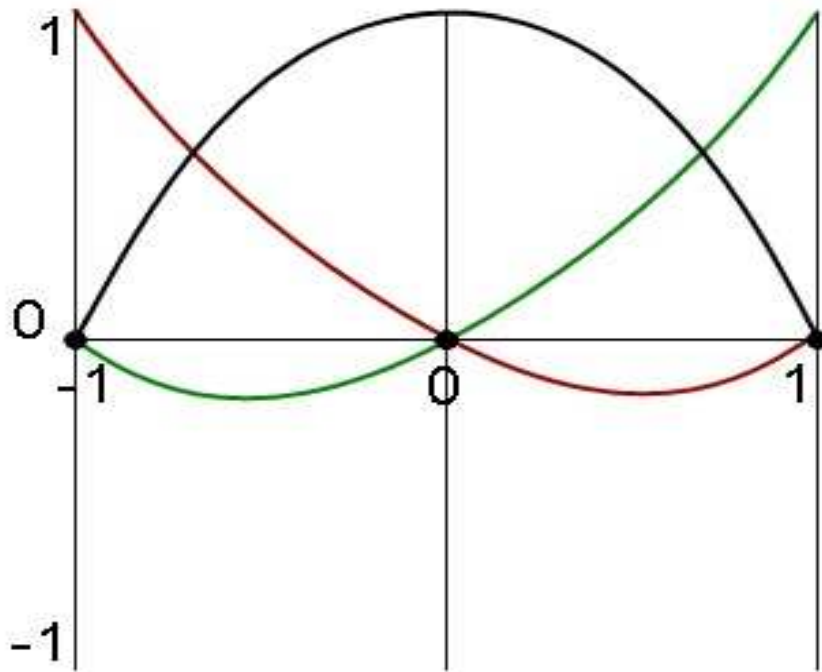
- Nodal

1. $1/2X^2 - 1/2X$
2. $1 - X^2$
3. $1/2X^2 + 1/2X$

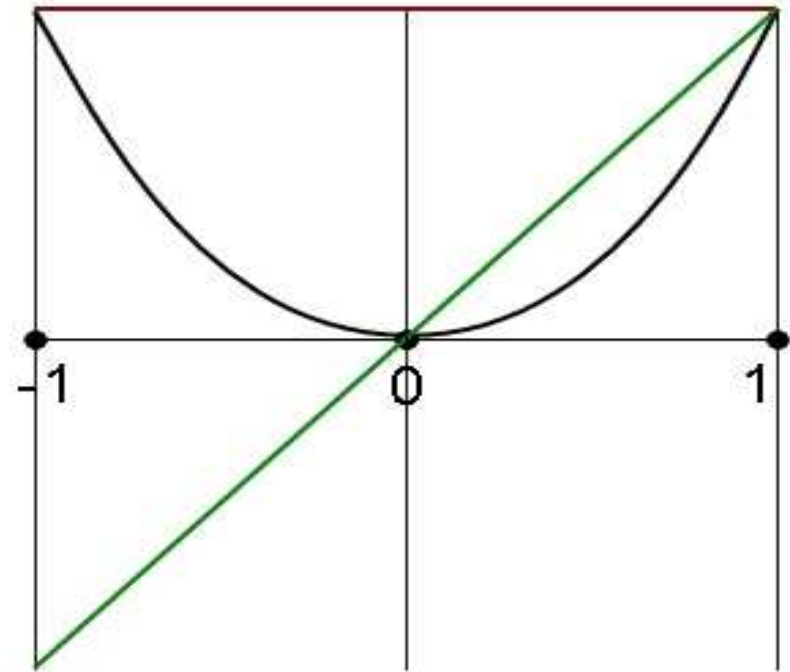
- Modal

1. X^2
2. X
3. 1

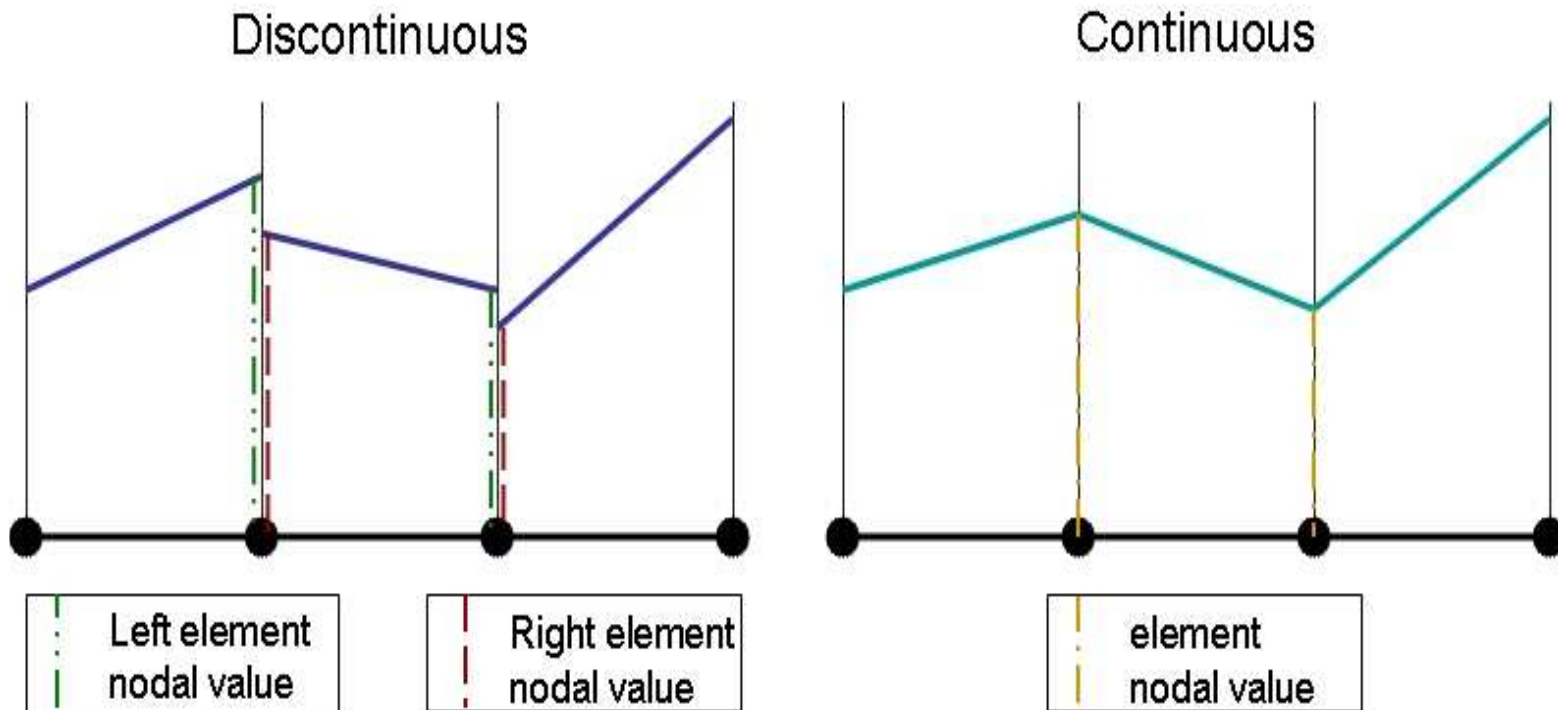
Nodal Basis

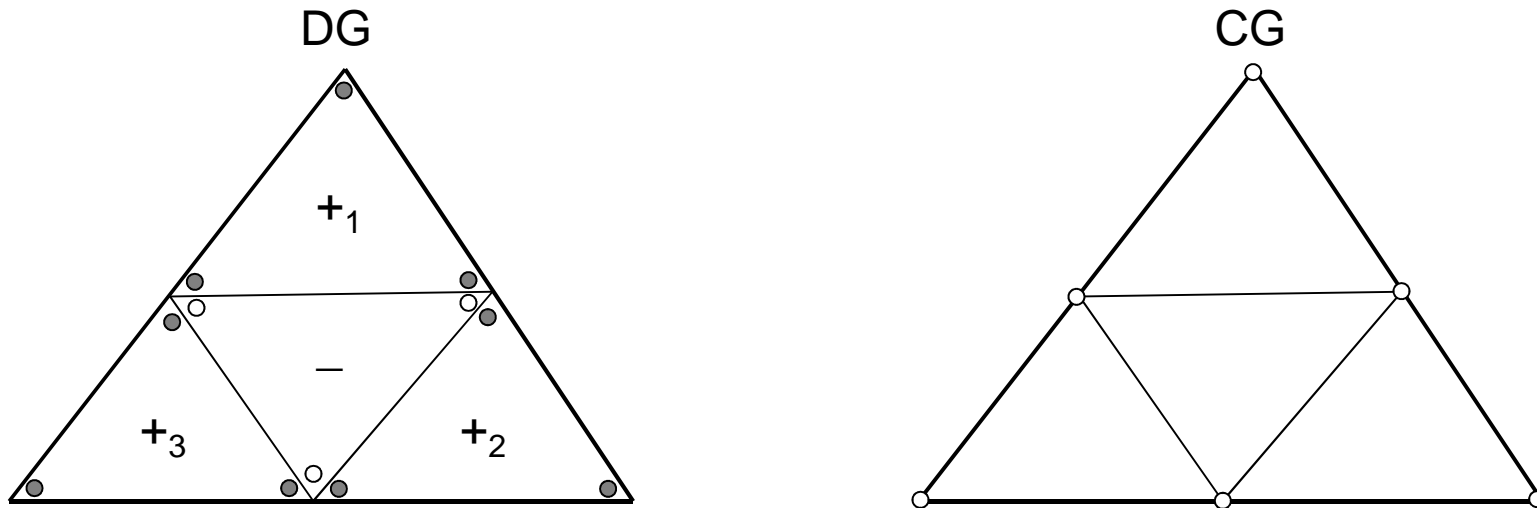


Modal Basis



- Continuous Function Space
- Discontinuous Function Space





- CG has continuity constraint at element edges
 - Forms matrix with many off-diagonal entries
 - Difficult to stabilize hyperbolic problems
- DG has no continuity constraint
 - Local solution in each element
 - Two unknowns on either side of element edges
 - Connection of domain achieved through fluxes: combination of unknowns on either side of edge
 - Forms matrix with block-diagonal structure

- Choose function space

$$W_h^p = \{w \in L^2(\Omega) : w|_K \in \mathcal{P}^p(K), \forall K \in \mathcal{T}_h\}$$

- Apply MWR

$$\frac{\partial u}{\partial t} + \nabla \cdot (\vec{c}u) = 0$$

$$\int_K w \frac{\partial u}{\partial t} dK + \int_K w \nabla \cdot (\vec{c}u) dK = 0$$

$$\int_K w \frac{\partial u}{\partial t} dK - \int_K \nabla w \cdot (\vec{c}u) dK + \int_K \nabla \cdot (\vec{c}uw) dK = 0$$

$$\int_K w \frac{\partial u}{\partial t} dK - \int_K \nabla w \cdot (\vec{c}u) dK + \int_{\partial K} w \hat{n} \cdot \vec{c}u d\partial K = 0$$

- Substitute in basis and test functions

$$\int_K w \frac{\partial u}{\partial t} dK - \int_K \nabla w \cdot (\vec{c}u) dK + \int_{\partial K} w \hat{n} \cdot \vec{c} \hat{u} d\partial K = 0$$

$$\int_K w \frac{\partial u_j}{\partial t} \theta_j dK - \int_K \nabla w \cdot (\vec{c}u_j \theta_j) dK + \int_{\partial K} w \hat{n} \cdot (\vec{c} \hat{u}_j \theta_j) d\partial K = 0$$

$$\int_K \theta_i \frac{\partial u_j}{\partial t} \theta_j dK - \int_K \nabla \theta_i \cdot (\vec{c}u_j \theta_j) dK + \int_{\partial K} \theta_i \hat{n} \cdot (\vec{c} \hat{u}_j \theta_j) d\partial K = 0$$

$$\frac{\partial u_j}{\partial t} \int_K \theta_i \theta_j dK - \vec{c}u_j \int_K \nabla \theta_i \cdot (\theta_j) dK + \vec{c} \hat{u}_j \cdot \int_{\partial K} \hat{n} (\theta_j \theta_i) d\partial K = 0$$

- Substitute for matrices
 - **M**- Mass matrix
 - **K**- Stiffness matrix or Convection matrix
- Solve specific case of 1D equations

$$\frac{\partial u_j}{\partial t} \int_K \theta_i \theta_j dK - \vec{c} u_j \int_K \nabla \theta_i \cdot (\theta_j) dK + \vec{c} \hat{u}_j \cdot \int_{\partial K} \hat{n}(\theta_j \theta_i) d\partial K = 0$$

$$\mathbf{M}_{ij} \frac{\partial u_j}{\partial t} - \mathbf{K}_{ij} \vec{c} u_j + \vec{c} \hat{u}_j \cdot \int_{\partial K} \hat{n}(\theta_j \theta_i) d\partial K = 0$$

$$1D : \quad \mathbf{M}_{ij} \frac{\partial u_j}{\partial t} - \mathbf{K}_{ij} \vec{c} u_j + \vec{c} \hat{u}_j \cdot \hat{n}(\theta_j \theta_i) = 0$$

$$1D : \quad u_j^{n+1} = u_j^n + \Delta t \mathbf{M}^{-1} (\mathbf{K}_{ij} \vec{c} u_j - \vec{c} \hat{u}_j \cdot \hat{n} \delta_{ij})$$

$$\hat{u}_j = \frac{u_j^+ + u_h^-}{2} - \frac{c}{|c|} \frac{u_j^+ - u_h^-}{2}$$

$$\frac{\partial u}{\partial t} + \nabla \cdot (\vec{c}u) = 0 \quad (1.1)$$

$$\int_K w \frac{\partial u}{\partial t} dK + \int_K w \nabla \cdot (\vec{c}u) dK = 0 \quad (1.2)$$

$$\int_K w \frac{\partial u}{\partial t} dK - \int_K \nabla w \cdot (\vec{c}u) dK + \int_K \nabla \cdot (\vec{c}uw) dK = 0 \quad (1.3)$$

$$\int_K w \frac{\partial u}{\partial t} dK - \int_K \nabla w \cdot (\vec{c}u) dK + \int_{\partial K} w \hat{n} \cdot \vec{c}u d\partial K = 0 \quad (1.4)$$

$$\int_K w \frac{\partial u_j}{\partial t} \theta_j dK - \int_K \nabla w \cdot (\vec{c}u_j \theta_j) dK + \int_{\partial K} w \hat{n} \cdot (\vec{c}u_j \theta_j) d\partial K = 0 \quad (1.5)$$

$$\int_K \theta_i \frac{\partial u_j}{\partial t} \theta_j dK - \int_K \nabla \theta_i \cdot (\vec{c}u_j \theta_j) dK + \int_{\partial K} \theta_i \hat{n} \cdot (\vec{c}u_j \theta_j) d\partial K = 0 \quad (1.6)$$

$$\frac{\partial u_j}{\partial t} \int_K \theta_i \theta_j dK - \vec{c}u_j \int_K \nabla \theta_i \cdot (\theta_j) dK + \vec{c}u_j \cdot \int_{\partial K} \hat{n} (\theta_j \theta_i) d\partial K = 0 \quad (1.7)$$

$$\mathbf{M}_{ij} \frac{\partial u_j}{\partial t} - \mathbf{K}_{ij} \vec{c}u_j + \vec{c}u_j \cdot \int_{\partial K} \hat{n} (\theta_j \theta_i) d\partial K = 0 \quad (1.8)$$

$$1D : \quad \mathbf{M}_{ij} \frac{\partial u_j}{\partial t} - \mathbf{K}_{ij} \vec{c}u_j + \vec{c}u_j \cdot \hat{n} (\theta_j \theta_i) = 0 \quad (1.9)$$

$$1D : \quad u_j^{n+1} = u_j^n + \Delta t \mathbf{M}^{-1} (\mathbf{K}_{ij} \vec{c}u_j - \vec{c}u_j \cdot \hat{n} \delta_{ij}) \quad (1.10)$$

$$\hat{u}_j = \frac{u_j^+ + u_h^-}{2} - \frac{c}{|c|} \frac{u_j^+ - u_h^-}{2} \quad (1.11)$$


```
clear all, clc, clf, close all

syms x
%create nodal basis
%Set order of basis function
%N >=2
N = 3;

%Create basis
if N==3
    theta = [1/2*x^2-1/2*x;
             1- x^2;
             1/2*x^2+1/2*x];
else
xi = linspace(-1,1,N);
for i=1:N
    theta(i)=sym('1');
    for j=1:N
        if j~=i
            theta(i) = ...
                theta(i)*(x-xi(j))/(xi(i)-xi(j));
        end
    end
end
end

%Create mass matrix
for i = 1:N
    for j = 1:N
        %Create integrand
        intgr = int(theta(i)*theta(j));
        %Integrate
        M(i,j) = ...
            subs(intgr,1)-subs(intgr,-1);
    end
end

%create convection matrix
for i = 1:N
    for j = 1:N
        %Create integrand
        intgr = ...
            int(diff(theta(i))*theta(j));
        %Integrate
        K(i,j) = ...
            subs(intgr,1)-subs(intgr,-1);
    end
end
```

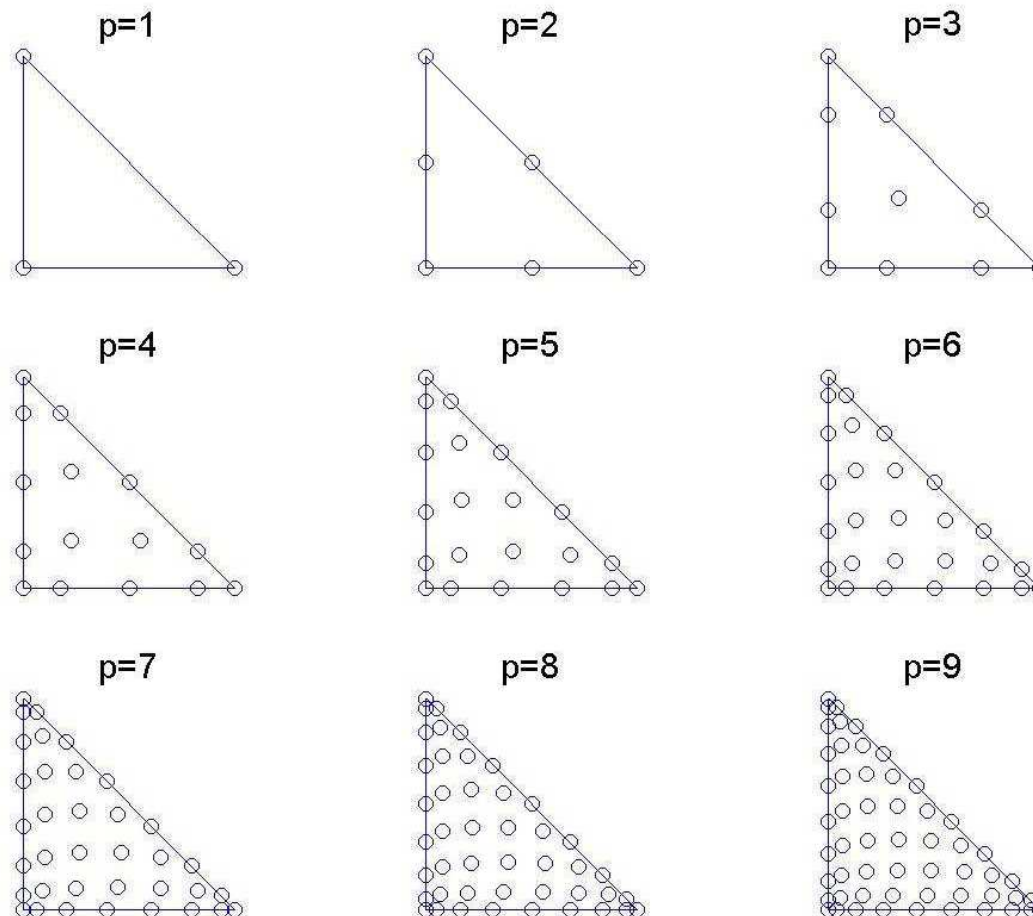
```
%% Initialize u
Nx = 20;
dx = 1./Nx;
%Multiply Jacobian through mass matrix.
%Note computational domain has length=2,
actual domain length = dx
M=M*dx/2;

%Create "mesh"
x = zeros(N,Nx);
for i = 1:N
    x(i,:) = ...
        dx/(N-1)*(i-1):dx:1-dx/(N-1)*(N-i);
end
%Initialize u vector
u = exp(-(x-.5).^2/.1^2);

%Set timestep and velocity
dt=0.002;    c=1;
%Periodic domain
ids = [Nx,1:Nx-1];
```

```
%Integrate over time
for i = 1:10/dt
    u0=u;
    %Integrate with 4th order RK
    for irk=4:-1:1
        %Always use upwind flux
        r = c*K*u;
        %upwinding
        r(end,:) = r(end,:) - c*u(end,:);
        %upwinding
        r(1,:) = r(1,:) + c*u(end,ids);
        %RK scheme
        u = u0 + dt/irk*(M\r);
    end
    %Plot solution
    if ~mod(i,10)
        plot(x,u, 'b')
        drawnow
    end
end
```

- How to create basis on triangles, tetrahedrals?
 - Need to create set of well-behaved Nodal point
- Integration in 2D, 3D?
 - Higher-order quadrature rules on triangles, tetrahedrals



- Higher-order derivatives
 - Naturally handled with CG
 - Somewhat more difficult with DG

$$\frac{\partial u}{\partial t} + \nabla \cdot \mathbf{F}_{inv}(u) + \nabla \cdot \mathbf{F}_{vis}(u, \nabla u) = S(u)$$

- Decompose higher derivatives into system of first-order derivatives

$$\frac{\partial u}{\partial t} + \nabla \cdot \mathbf{q} = 0, \quad \text{in } (0, T) \times \Omega$$

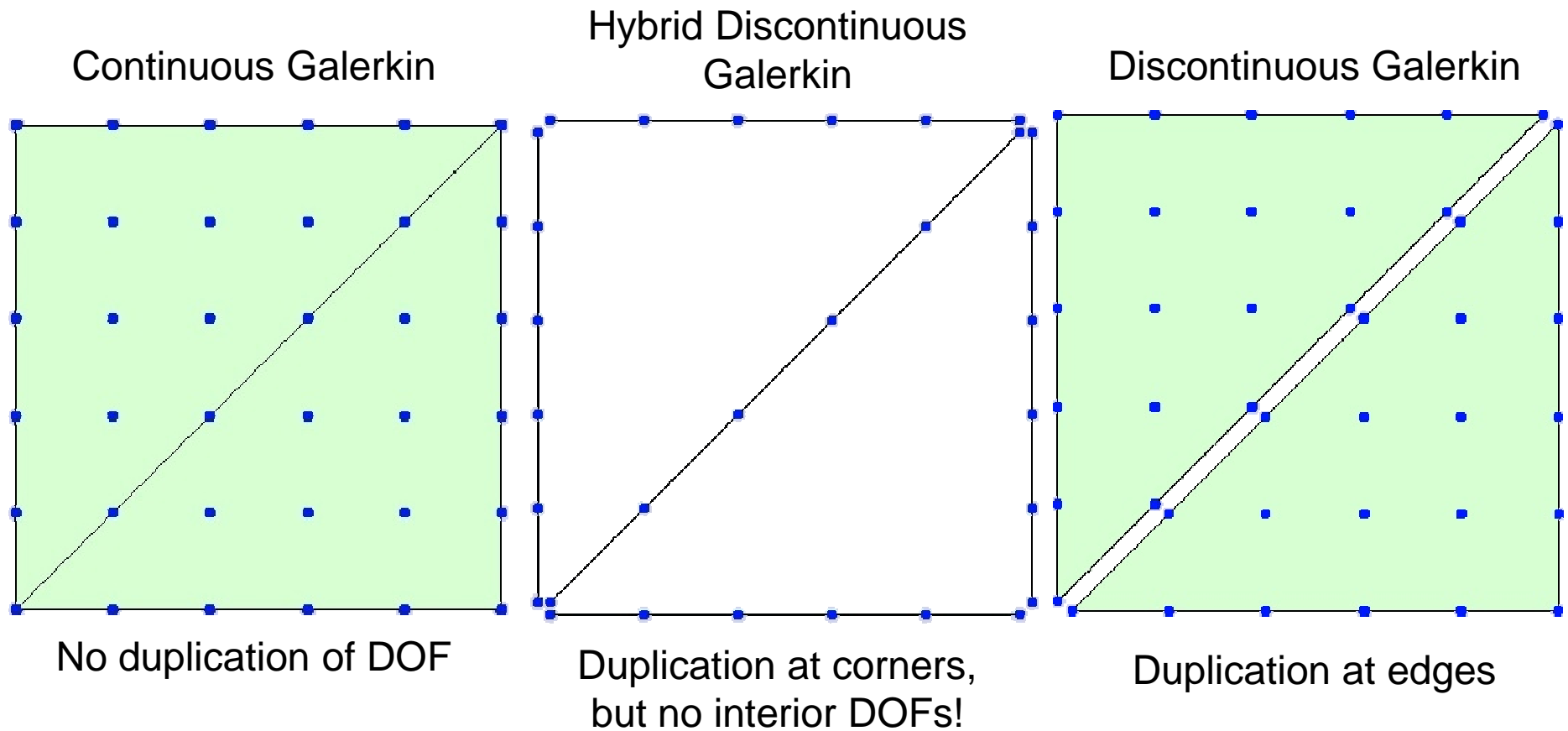
$$\mathbf{q} + \kappa \nabla u = 0, \quad \text{in } \Omega$$

$$u = g_D, \quad \text{on } \partial\Omega_D$$

$$\mathbf{q} \cdot \hat{\mathbf{n}} = g_N, \quad \text{on } \partial\Omega_N$$

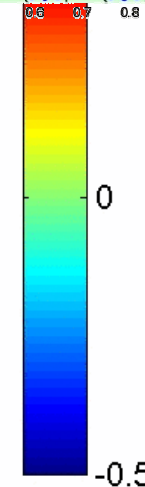
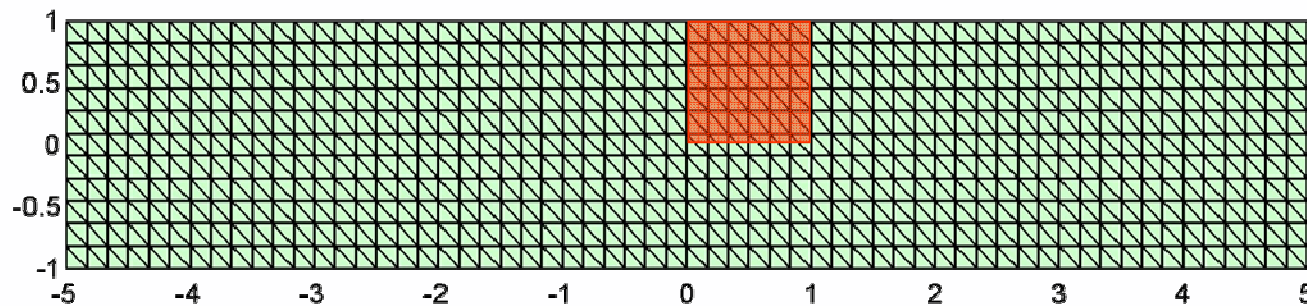
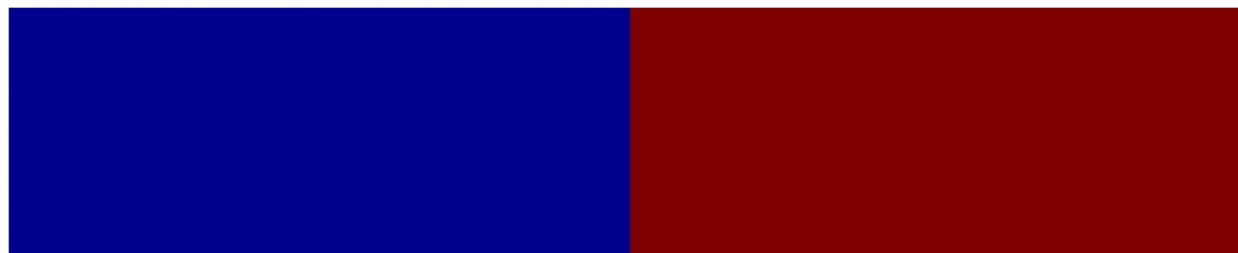
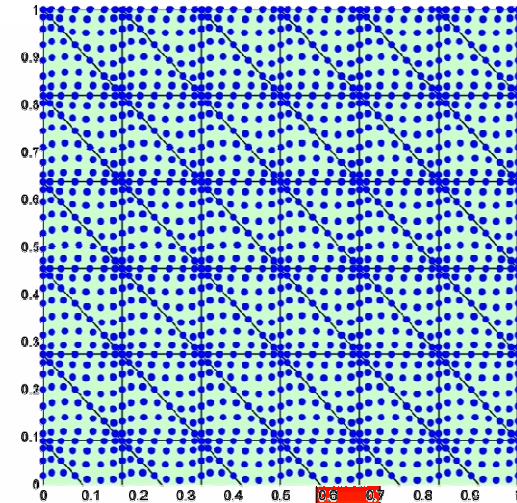
$$u = u_0, \quad \text{in } (0, 0) \times \Omega$$

- Research directed towards improved treatment of higher-order derivatives



- 37,000 DOF, 14,000 HDG unknowns
- 13.5 hrs
- 1320 Elements
- $p=6$
- $Gr = 1.25 \times 10^6$, $Sc=0.71$

time: 0
 ρ

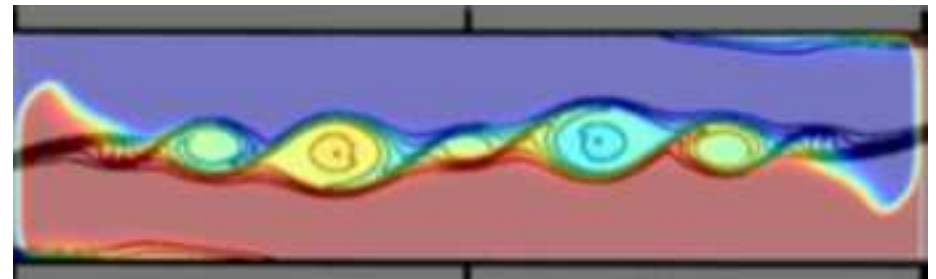
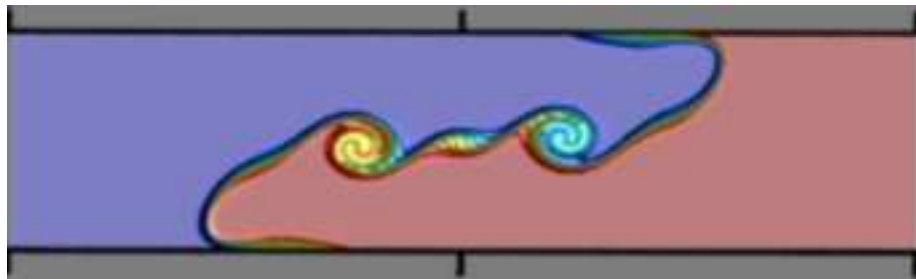
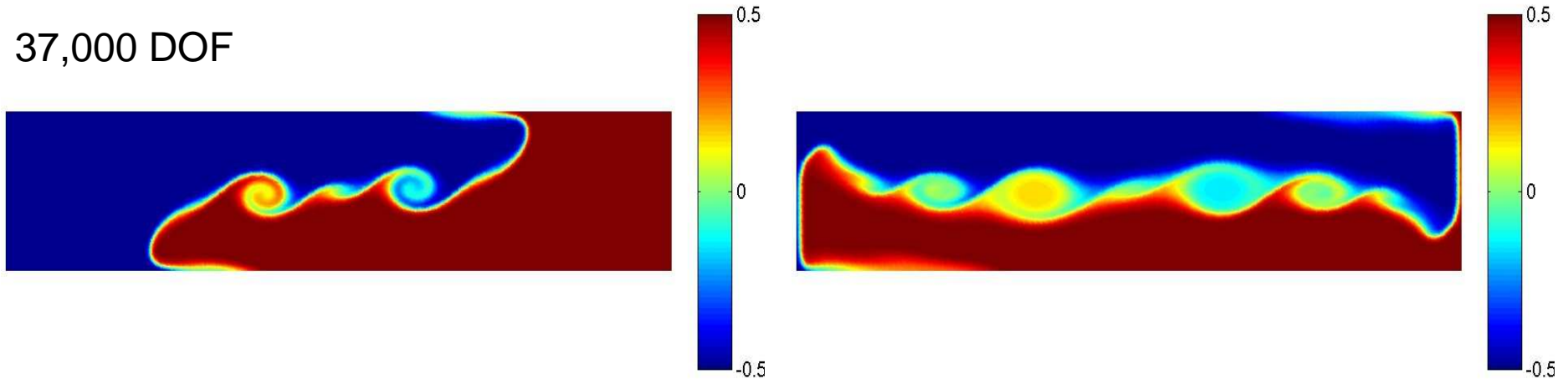


Hartel, C., Meinburg, E., and Freider, N. (2000). *Analysis and direct numerical simulations of the flow at a gravity-current head. Part 1. Flow topology and front speed for slip and no-slip boundaries.* J. Fluid. Mech, 418:189-212.

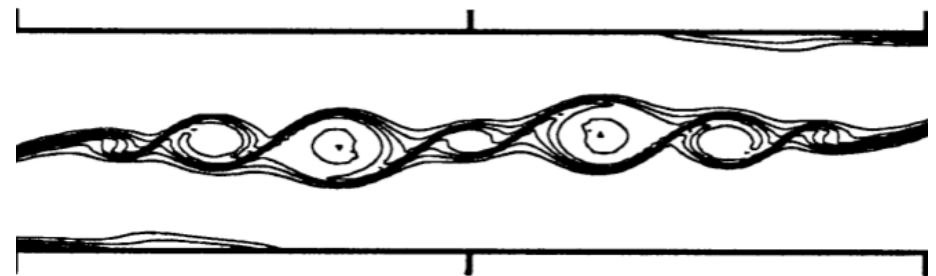
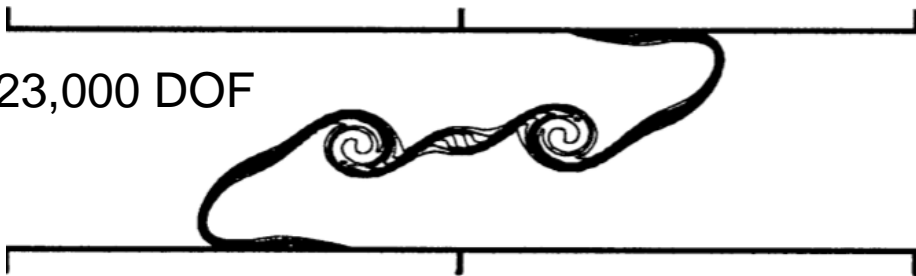
Time = 5

Time = 10

37,000 DOF



23,000 DOF



Hartel, C., Meinburg, E., and Freider, N. (2000). *Analysis and direct numerical simulations of the flow at a gravity-current head. Part 1. Flow topology and front speed for slip and no-slip boundaries.* J. Fluid. Mech, 418:189-212.

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